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## Inverse Optimum Safety Factor Method for Reliability-Based Topology Optimization Applied to Free Vibrated Structures

G. Kharmanda<sup>1</sup>, I. R. Antypas<sup>2\*</sup>, A. G. Dyachenko<sup>2</sup>

<sup>1</sup>*National Institute of Applied Sciences of Rouen  
(Saint-Étienne-du-Rouvray, France)*

<sup>2</sup>*Don State Technical University (Rostov-on-Don, Russia)*

\**imad.antypas@mail.ru*

**Introduction.** The classical topology optimization leads to a prediction of the structural type and overall layout, and gives a rough description of the shape of the outer as well as inner boundaries of the structure. However, the probabilistic topology optimization (or reliability-based topology optimization) model leads to several reliability-based topologies with high performance levels. The objective of this work is to provide an efficient tool to integrate the reliability-based topology optimization model into free vibrated structure.

**Materials and Methods.** The developed tool is called inverse optimum safety method. When dealing with modal analysis, the choice of optimization domain is highly important in order to be able to eliminate material taking account of the constraints of fabrication and without affecting the structure function. This way the randomness can be applied on certain boundary parameters.

**Results.** Numerical applications on free vibrated structures are presented to show the efficiency of the developed strategy. When considering a required reliability level, the resulting topology represents a different topology relative to the deterministic resulting one.

**Discussion and Conclusion.** In addition to its simplified implementation, the developed inverse optimum safety factor strategy can be considered as a generative tool to provide the designer with several solutions for free vibrated structures with different performance levels.

**Keywords:** deterministic topology optimization, reliability-based topology optimization, modal analysis, optimum safety factor, optimization domain

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## Метод обратного оптимального фактора безопасности для оптимизации топологии на основе надежности применительно к свободным вибрирующим структурам

Г. Харманда<sup>1</sup>, И. Р. Антибас<sup>2\*</sup>, А. Г. Дьяченко<sup>2</sup>

<sup>1</sup>Национальный институт прикладных наук Руана  
(г. Сент-Этьен-дю-Рувре, Франция)

<sup>2</sup>ФГБОУ ВО «Донской государственный технический университет» (г. Ростов-на-Дону, Россия)

\**imad.antypas@mail.ru*

*Введение.* Классическая оптимизация топологии приводит к предсказанию структурного типа и общей компоновки и дает примерное описание как внешних, так и внутренних границ форм структуры. Однако вероятностная модель оптимизации топологии (или оптимизационная топология на основе надежности) приводит к нескольким вариантам решения надежности на основе топологии с высоким уровнем производительности. Цель данной статьи – создать эффективный инструмент для интеграции модели оптимизации топологии на основе надежности для свободных вибрирующих структур.

*Материалы и методы.* Разработанный инструмент называется методом обратной оптимальной безопасности. При использовании модального анализа выбор области оптимизации очень важен для обеспечения возможности снижения материалоемкости с учетом ограничений в изготовлении и без влияния на ее структурную функцию. Таким образом, случайность может быть применена к некоторым граничным параметрам.

*Результаты исследования.* Представлены численные приложения на свободных вибрирующих структурах, показывающие эффективность разработанной стратегии. При рассмотрении требуемого уровня надежности результирующая топология представляет другую топологию относительно детерминированной результирующей.

*Обсуждение и заключение.* В дополнение к своей упрощенной реализации разработанная обратная оптимальная стратегия фактора надежности может рассматриваться как генеративный инструмент, обеспечивающий проектировщику несколько вариантов решений для свободно вибрирующих конструкций с различными уровнями производительности.

**Ключевые слова:** оптимизация детерминированной топологии, оптимизация топологии на основе надежности, модальный анализ, оптимальный фактор безопасности, домен оптимизации

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### Introduction

Topology optimization attempts to answer one of the first questions concerning the nature of the structure to fulfill the necessary technical specifications. The topology problem would then consist of determining the structure's general characteristics, and the goal of topology

optimization would be to make that initial choice as automatically as possible [1]. In addition, when using topology optimization concepts, both macroscopic structures and microscopic materials can be found. In other word, we determine not only the optimal spatial material layout distribution at the macroscopic structural scale, but also

the optimal local use of the cellular material at the microscopic scale<sup>1</sup>.

In the literature, two main models of topology optimization can be distinguished: deterministic model and probabilistic (or reliability-based) one. In Deterministic Topology Optimization (DTO), a single solution for a given domain can be searched<sup>2</sup>. However, the Reliability-Based Topology Optimization (RBTO) model developed in this paper can lead to several solutions with different advantages. It enables us to choose the best solution to fulfill the technical specifications. The structural weight of the resulting topologies obtained by this model is reduced in comparison to the DTO model. In addition, when using the RBTO model, the structure obtained is more reliable compared to deterministic topology for the same weight levels<sup>3</sup>. Two points of view are presented for the development of this model: topology optimization and reliability analysis. A literature review is established in the next section, to show the different advantages of the RBTO model.

### Literature Review

The main difference between deterministic topology optimization and reliability-based topology optimization is to consider the hazards about the parameters having important roles for optimal topology. The main idea of the RBTO is based on the Reliability-Based Design Optimization (RBDO). In a RBDO problem, the uncertainties regarding the sizing variables are taken into account in order to ensure greater reliability of the proposed

solution. However, the RBTO seeks to provide designers with several solutions that have several reliability levels. This way the designer can select best solution. In the Reliability-Based Design Optimization (RBDO), several methods have been developed. The different developments can be classified in two points of view:

From point of view “topology optimization”, Kharmanda and Olhoff<sup>4</sup> have elaborated an RBTO model with object of providing the designer with several reliability-based structures however in the classical topology optimization, the designer produces only one deterministic topology. It has been shown the importance of the RBTO model yields structures that are more reliable than those produced by deterministic topology optimization (for the same weight, see also<sup>5</sup> [2; 3]). In the RBTO model reliability constraints have been introduced into deterministic topology optimization problem. The initial sensitivity analysis is used to identify random variables which have significant effect on the objective function and the limit state function used is a linear combination of the random variables. Therefore, the proposed approach is a heuristic strategy that aims to reduce mass while improving the reliability level of the structure without greatly increasing its weight. But the limit state function used by them was not based on failure criteria for the structure. This formulation considered uncertainty with respect to geometrical dimension and applied load only. Also their reliability analysis seems to be independent of the boundary and loading condition, so

<sup>1</sup> Xia L. Multiscale structural topology optimization. ISTE–Elsevier, 2016. Available at: <https://www.sciencedirect.com/book/9781785481000/multiscale-structural-topology-optimization>

<sup>2</sup> Zhang W., Zhu J., Gao T. Topology optimization in engineering structure design. ISTE–Elsevier, 2016. Available at: <https://www.sciencedirect.com/book/9781785482243/topology-optimization-in-engineering-structure-design>

<sup>3</sup> Kharmanda G., El-Hami A. Biomechanics optimization, uncertainties and reliability. ISTE–Wiley, 2017. Available at: <http://ebook-dl.com/book/8163>

<sup>4</sup> Kharmanda G., Olhoff N. Reliability-based topology optimization: Report. Aalborg: Aalborg University, 2001. Available at: <http://www.forskningsdatabasen.dk/en/catalog/2389380317>

<sup>5</sup> Kharmanda G., Olhoff N. Reliability-based topology optimization as a new strategy to generate different structural topologies. In: E. Lund, N. Olhoff, J. Stegmsen (Eds.) 15th Nordic Seminar in Computational Methods. Aalborg: Aalborg University, 2002. p. 11-14. Available at: [https://www.researchgate.net/publication/237295035\\_Reliability-Based\\_Topology\\_Optimization\\_as\\_a\\_New\\_Strategy\\_to\\_Generate\\_Different\\_Structural\\_Topologies](https://www.researchgate.net/publication/237295035_Reliability-Based_Topology_Optimization_as_a_New_Strategy_to_Generate_Different_Structural_Topologies)

their results showed similar values for the uncertain variables for different structures. Next, Patel and Choi [4] used probabilistic neural networks in the case of highly non-linear or disjoint failure domain problems. This strategy has been efficiently applied on different truss structures. Recently, Wan et al. [5] developed a non-probabilistic reliability-based topology optimization method for detailed design of continuum structures, in which the unknown but bounded uncertainties (UBB) existing in material and external loads are considered simultaneously. Their results show that considering the UBB uncertainty effects during the whole procedure of topology optimization may have a significant influence on the final structural configurations.

From a point of view “reliability analysis”, the classical topology optimization is formulated as finding the stiffest structural layout with a volume constraint. Here, the feasibility of volume constraint is not critical in structural design problems. It is more important to consider the variations of the stiffness under uncertainties. To maintain the robustness of stiffness in the topology design, Bae and Wang [6] formulated the topology design optimization as volume minimization problem with a displacement constraint and applied the RBDO technique. They minimize the structural volume subject to linear limit state function. In the research of, the extension of the work of Bae and Wang for the geometrically non linear problems is studied or reformulated to avoid repetition. They minimize the structural volume subject to a nonlinear limit state function. Next, Patel et al. [7] have developed the Hybrid Cellular Automaton (HCA) method for structural synthesis of continuum material where the state of each cell

is defined by both density and strain energy. In<sup>6</sup>, a decoupled RBDO approach is employed such that the topology optimization is separate from the reliability analysis [7] showed the use of RBTO using the gradient free Hybrid Cellular Automata (HCA) method. Their formulation incorporates uncertainty with respect to material property also. They considered limit state function based on failure modes on the output displacements. Eom et al. [8] performed the RBTO model using bi-directional evolutionary structural optimization and the standard response surface method. Jalalpour and Tootkaboni [9] developed a computationally method for reliability-based topology optimization for continuum domains under material properties uncertainty.

Comparing both different points of view, RBTO methods from a point of view “reliability analysis” are inherently computationally expensive because of additional required system analysis associate with RBDO since a large number of design variables are associated with continuum topology optimization problems<sup>7</sup>.

So the point of view “topology optimization” seems to be interesting for topology designers because it provides several reliability-based structures relative the reliability index changes. It leads to different layout structures while the developments from a point of view “reliability analysis” leads to same layout structures with different densities that have no sense for the following optimization stages [10].

To perform the RBTO problems, different RBDO techniques can be used since we deal with different problem definition or philosophy. Several RBDO methods have been developed regarding to their use<sup>8, 9</sup> [11]. For example, the OSF

<sup>6</sup> Agarwal H. Reliability based design optimization: formulations and methodologies: Ph.D. Thesis. Notre Dame : University of Notre Dame, 2004. Available at: <http://adsabs.harvard.edu/abs/2004PhDT.....148A>

<sup>7</sup> Kharmanda G., El-Hami A. Biomechanics optimization, uncertainties and reliability. ISTE–Wiley, 2017. Available at: <http://ebook-dl.com/book/8163>

<sup>8</sup> Ibid.

<sup>9</sup> Yaich A., Kharmanda G., El Hami A., Walha L., Haddar A. Reliability based design optimization under fatigue damage constraints of structures subject to random vibrations. In: ECSO2017: European Conference on Stochastic Optimization. 2017. p. 20-22.

method as an efficient RBDO tool, has been simply implemented by performing two main stages [12]. The first stage is to find the failure point (design point) using a simple optimization process while the second stage consists of using the OSF formulations to find the optimum solution. In this work, for the RBTO model, the developed Inverse Optimum Safety (IOSF) method consists of first finding the configuration using Deterministic Topology Optimization (DTO). Next, the OSF formulations [12] are used with inverse derivative signs in order to provide several reliability-based topologies. The resulting topologies are controlled by a given design space (loading, material, geometry, meshing...). In the modal analysis, there is no applied loads. So the integration of topology optimization into free vibrated structures may lead to unrealistic topologies. Therefore, the choice of optimization domain is highly important in order to be able to eliminate material taking account of the constraints of fabrication and without affecting the structure function. For this purpose, several choices are carried out to demonstrate the importance of optimization domains relative to the static studies [3] where the used boundary conditions can lead to admissible topologies.

### Materials and Methods

#### *Deterministic Topology Optimization*

The topology optimization problem relates to the minimization of the strain energy, subject to the limitation of the structural volume<sup>10</sup>. All the loading parameters and material properties are considered deterministic. The topology optimization problem is to minimize the compliance, subject to a target percentage value of volume  $f$ . This problem can be mathematically written as follows:

$$\begin{aligned} \min : & \text{Comp} \\ \text{s.t.} : & \frac{V}{V_0} \leq f, \end{aligned} \quad (1)$$

where *Comp* is the compliance considering the material densities in each element as optimization variables that belong to the interval [0, 1].  $V_0$  and  $V$  are the initial and current volume values. Formulation (1) is a basic form and can be used with several topology optimization methods such as SIMP (Solid Isotropic Microstructure with Penalty), homogenization approach, ... [13; 14].

#### *Reliability-Based Topology Optimization*

In deterministic structural optimization, the designer aims to reduce the construction cost without taking into account the effects of uncertainties concerning materials, geometry and loading. This way, the resulting optimal configurations may represent a lower reliability level and then leads to higher failure rate. The balance between the cost minimization and the reliability maximization is a great challenge for the designer. The importance of the reliability criteria on the deterministic design optimization is to improve the reliability level in the system without largely increasing its weight. Thus, when integrating the reliability concept into the sizing and shape optimization, the model is called Reliability-Based Design Optimization (RBDO), which allows us to design structures, which satisfy economy and safety requirements. But when coupling the reliability analysis with the topology optimization being considered non-quantitative of nature. The coupling model is called Reliability-Based Topology Optimization (RBTO) [15]. The purpose of the Reliability-Based Topology Optimization (RBTO) is to consider some uncertainties of the geometry or the loading of the structure, by introducing the reliability criteria in the optimization procedure. This integration takes into account the randomness of the applied loads and the geometry description. The RBTO problem is generally written as:

<sup>10</sup> Rozvany G.I.N. Problem classes, solution strategies and unified terminology of FE-based topology optimization. In: Rozvany G.I.N., Olhoff N. (Eds.) Topology Optimization of Structures and Composite Continua. Dordrecht: Kluwer, 2000. p. 19-35.

$$\begin{aligned} \min & : \text{Comp} \\ \text{s.t.} & : \beta \geq \beta_t \\ \text{and} & : \frac{V}{V_0} \leq f_t, \end{aligned} \quad (2)$$

where  $\beta$  and  $\beta_t$  are the reliability index of the system and the target reliability index, respectively (for more information about reliability methods, see<sup>11</sup> [16]). The integration of reliability analysis into the topology optimization has been carried out by performing two decoupled problems for static studies [2]. However, in this work, an efficient method called Inverse Optimum Safety method, is developed and applied to free vibrated structures considering the design domain uncertainty.

$$u_i^* = \beta_t \sqrt{\frac{\left| \frac{\partial G}{\partial y_i} \right|}{\sum_{j=1}^n \left| \frac{\partial G}{\partial y_j} \right|}}, \quad i = 1, \dots, n, \quad (3)$$

where the sign of  $\pm$  depends on the sign of the derivative of the limit state function with respect to random vector  $y_i$ , i. e.,

$$\frac{\partial G}{\partial y_i} > 0 \Leftrightarrow u_i^* > 1. \quad (4)$$

Considering that the random variable vector follows the normal distribution law, the safety factor can be written as follows<sup>12</sup> [16]:

$$S_{f_i} = 1 + \gamma_i \cdot u_i^*, \quad i = 1, \dots, n, \quad (5)$$

where the variance coefficient  $\gamma_i$  relating the mean  $m_i$  and standard-deviation  $\sigma_i$  equals to:  $\gamma_i = \sigma_i/m_i$ .

However, the idea of the developed IOSF is to find a resulting deterministic topology  $P_y^*$  considered as a failure point, and next we seek a reliability-based topology  $P_x^*$  that should be more reliable than the first solution  $P_y^*$ , as well as should respect a required reliability level  $\beta_t$ . So the failure point  $P_y^*$  is found by a DTO procedure and the reliability-based topologies  $P_x^*$  are found using the OSF formulations but with inverse derivative signs (formulation 4). This strategy generates several reliability-based topologies according to the reliability index values. The generation of several topologies is controlled by a sensitivity analysis being an efficient indicator to find the role of each parameter.

**Results**

In this section, the topology optimization is applied to a 2D cantilever beam (dimensions: 200 × 50 mm) to find the best distribution of material. The material in this beam is steel, which has a Young’s modulus  $E = 200\,000\text{ MPa}$  and a Poisson’s ratio equal to:  $\nu = 0.3$ . The density of the material is  $\rho = 7.190 \times 10\text{ Kg/mm}$ . The behavior of the material is linear elastic isotropic. The objective is to perform topology optimization to obtain the best distribution of the materials. The topology optimization problem is to minimize the compliance of the structure, subject to the volume fraction 50 %. To carry out topology optimization, the meshing model is constructed using the nonlinear element (PLANE82 – 8-node) and the used method is the Optimality Criteria (OC) implemented in ANSYS Software.

When considering the modal studies, the choice of optimization domain is very important in order to be able to eliminate material taking account of the constraints of fabrication and without affecting the function of the resulting cantilever beam.

<sup>11</sup> Kharmanda G., Antypas I. Integration of reliability and optimization concepts into composite yarns. In: 10<sup>th</sup> International Scientific-Practical Conference of Current Status and Prospects of Agricultural Engineering, “INTERAGROMASH-2017”. Rostov-on-Don: DSTU Publ. Centre; 2017. p. 174-176.

<sup>12</sup> Kharmanda G., El-Hami A. Biomechanics optimization, uncertainties and reliability. ISTE–Wiley, 2017. Available at: <http://ebook-dl.com/book/8163>

For this purpose, we optimize several cases in order to first demonstrate the importance of the initial design domain and then show the advantages and disadvantages of each model.

#### Model 1

Fig. 1, a–b respectively show the geometric model of the studied beam and the resulting topology, considering the entire geometry as an optimization domain  $A_1$  (i. e. the domain to be optimized).

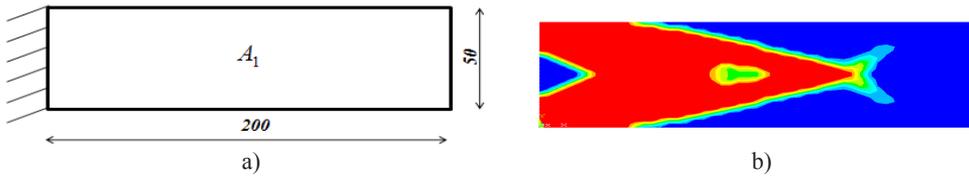


Fig. 1. Configurations of model 1 when considering deterministic topology optimization: a) a cantilever beam with a single optimized area; b) resulting topology

Р и с. 1. Конфигурация модели 1 при рассмотрении оптимизации детерминированной топологии: а) консольная балка с одной оптимизированной областью; б) результирующая топология

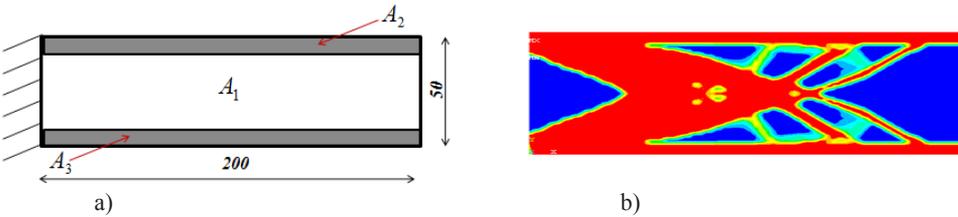


Fig. 2. Configurations of model 2 when considering deterministic topology optimization: a) a cantilever beam with double non-optimized areas; b) resulting topology

Р и с. 2. Конфигурация модели 2 при рассмотрении оптимизации детерминированной топологии: а) консольная балка с двойными неоптимизированными областями; б) результирующая топология

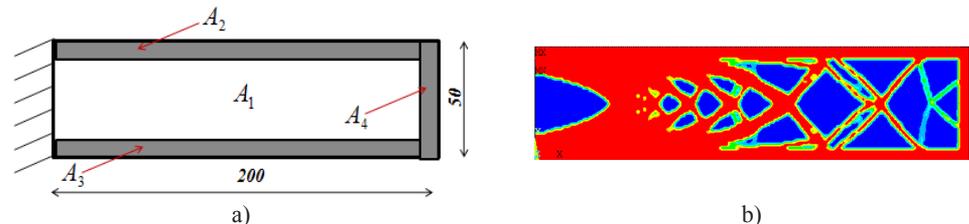


Fig. 3. Configurations of model 3 when considering deterministic topology optimization: a) a cantilever beam with triple non-optimized areas; b) resulting deterministic topology optimization

Р и с. 3. Конфигурация модели 3 при рассмотрении оптимизации детерминированной топологии: а) консольная балка с тройными неоптимизированными областями; б) результирующая оптимизация детерминированной топологии

#### Model 2

Fig. 2, a shows the geometric model of the studied beam, considering middle part as the optimization domain  $A_1$  and the upper and lower parts as the domain not to be optimized ( $A_2$  and  $A_3$ ). Fig. 2, b shows the corresponding resulting topology.

#### Model 3

Fig. 3 shows the geometric model of the studied beam, considering inner part as the optimization domain  $A_1$ , the upper,

lower and lateral parts as the domain not to be optimized ( $A_2$ ,  $A_3$  and  $A_4$ ).

Here, the dimensions ( $x_1$ ,  $x_2$ ,  $x_3$ ) of non-optimized domain of the third model are considered as random variables (see fig. 4, a). At the initial point, these variables

equal to: 5 mm. The target reliability index is equal to  $\beta_t = 3$  and that the proportion of the standard deviations compared to the average values is equal to<sup>13</sup>. Fig. 3, b and 4, b show the corresponding resulting DTO and RBTO configurations, respectively.

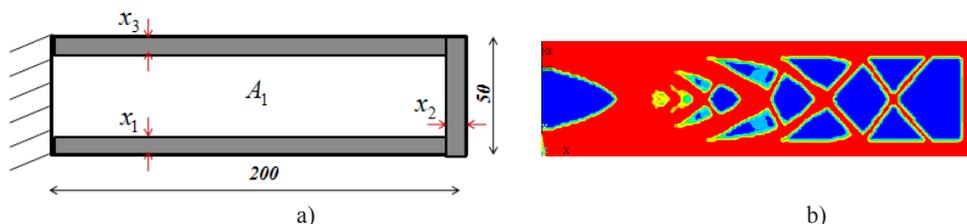


Fig. 4. Configurations of model 3 when considering reliability-based topology optimization: a) initial design with 3 random variables; b) resulting reliability-based topology optimization

Р и с. 4. Конфигурация модели 3 при рассмотрении оптимизации топологии на основе надежности: а) первоначальная конструкция с 3 случайными величинами; б) результирующая оптимизация топологии на основе надежности

Table 1  
Таблица 1

**Reliability-based topology optimization results**  
**Результаты оптимизации топологии на основе надежности**

Parameters / Параметры	Thickness of lower part $x_1$ / Толщина нижней части $x_1$	Thickness of lateral part $x_2$ / Толщина боковой части $x_2$	Thickness of upper part $x_3$ / Толщина верхней части $x_3$
Failure point $P_y^*$ / Точка отказа $P_y^*$	5.00	5.00	5.00
Compliance $Comp$ / Соответствие $Comp$	1.37700	1.37766	1.37766
Compliance sensitivity $\partial C / \partial y_i$ / Соблюдение чувствительности $\partial C / \partial y_i$	-0.020	-0.018	-0.025
Normalized vector $u_i^*$ / Нормализованный вектор $u_i$	1.683	1.626	1.877
Optimum safety factors $S_{f_i}$ / Оптимальные факторы безопасности $S_{f_i}$	1.420	1.407	1.469
Optimum point $P_x^*$ / Оптимальная точка $P_x^*$	7.10	7.03	7.35

<sup>13</sup> Ibid.

Table 1 presents the different parameters concerning the failure point  $P_y^*$  and the optimum point  $P_x^*$  considering the target reliability index  $\beta_t = 3$ .

At the failure point  $P_y^*$ , the normalized vector  $u_i^*$  is evaluated according to formulation (3) considering the central finite difference technique to evaluate the required derivatives of the compliance  $\partial C / \partial y_i$ <sup>14</sup>. The safety factors  $S_{f_i}$  are next computed according to formulation (5) and the corresponding reliability-based topology is finally evaluated at the optimum point  $P_x^*$ .

### Discussion and Conclusion

According to our previous [2; 3], when considering a static case, the loading and the fixation can control the external geometrical boundaries. However, when considering the modal studies, the choice of optimization domain is very important in order to be able to eliminate material taking account of the constraints of fabrication and without affecting the function of the resulting structures. Three models with different optimization domains are studied to show the effect of the optimization domain choice.

For the first model, when considering the entire geometry as an optimization domain, the resulting topology changes totally the external geometry and then affects its function. Fig. 1, b shows that the cantilever beam length is reduced which can totally change the detailed design stage. Therefore, the initial design domain should be modified to attend the design objectives. For second model, the upper and lower parts are considered as non-optimized domains. This way the resulting topology is better than the first model but some other failure scenarios can occur at the right region. However, in the

third model, all free boundaries are considered as non-optimized domains. The resulting topology will not affect beam function. Here, the DTO algorithm leads to a single topology considering a given initial design space while the RBTO algorithm leads two several topologies relative to the reliability index values.

The main different between the IOSF and OSF method is to invert the sign of the derivatives is inverted. Here, the mean values are considered to be the failure point  $P_y^*$ , and the objective is to increase the reliability level starting from this point. The resulting DTO configuration leads to weak sections (fig. 3, b) and meets difficult fabrication constraints while the RBTO configuration (fig. 4, b) is much more reliable than that produced by DTO.

In general, the choice of the initial domain depends on the designer experience and may lead to several failure scenarios. A reliability concept can be integrated during the optimization process in order to control the resulting topology performance and to generate several reliability-based topologies. In this problem, when applying the IOSF method to obtain a layout which respects a required reliability level, a different topology is obtained. The advantage of this strategy is to produce different topology with additional computing cost regarding the reliability stage.

Thus, reliability-based topology optimization is able to generate multiple topologies, giving the designer a range of solutions by adding certain reliability constraints. The efficiency of the developed IOSF method is to perform the RBTO in a single loop relative to the previous method proposed by [2] which also needs double loops.

<sup>14</sup> Ibid.

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*About authors:*

**Ghias Kharmanda**, Researcher, Mechanics Laboratory of Normandy, National Institute of Applied Sciences of Rouen (685 University Avenue, Saint-Étienne-du-Rouvray 76801, France), ResearcherID: O-6690-2018, ORCID: <https://orcid.org/0000-0002-8344-9270>, [g.kharmanda@gmail.com](mailto:g.kharmanda@gmail.com)

**Imad R. Antypas**, Associate Professor, Chair of Design Principles of Machines, Don State Technical University (1 Gagarin Square, Rostov-on-Don 344000, Russia), Ph.D. (Engineering), ResearcherID: O-4789-2018, ORCID: <https://orcid.org/0000-0002-8141-9529>, [imad.antypas@mail.ru](mailto:imad.antypas@mail.ru)

**Alexey G. Dyachenko**, Associate Professor, Chair of Design Principles of Machines, Don State Technical University (1 Gagarin Square, Rostov-on-Don 344000, Russia), Ph.D. (Engineering), ResearcherID: O-4796-2018, ORCID: <https://orcid.org/0000-0001-9934-4193>, [dyachenko\\_aleshka@bk.ru](mailto:dyachenko_aleshka@bk.ru)

*Contribution of the authors:*

G. Kharmanda – scientific guidance, statement of the problem, definition of research methodology, collection and analysis of analytical and practical materials on the research topic, critical analysis and finalization of the solution, computer realization of the solution of the problem; I. R. Antypas – statement of the problem, definition of research methodology, collection and analysis of analytical and practical materials on the research topic; A. G. Dyachenko – analysis of scientific sources on the topic of research, critical analysis and revision of the text.

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*Об авторах:*

**Харманда Гиас**, исследователь, лаборатория механики Нормандии, Национальный институт прикладных наук Руана (76801, Франция, г. Сент-Этьен-дю-Рувре, Авеню-дель-Университе, д. 685), доктор философии по техническим наукам, ResearcherID: O-6690-2018, ORCID: <https://orcid.org/0000-0002-8344-9270>, [g.kharmanda@gmail.com](mailto:g.kharmanda@gmail.com)

**Антибас Имад Ризакалла**, доцент кафедры основ конструирования машин, ФГБОУ ВО «Донской государственный технический университет» (344000, Россия, г. Ростов-на-Дону, пл. Гагарина, д. 1), кандидат технических наук, ResearcherID: O-4789-2018, ORCID: <https://orcid.org/0000-0002-8141-9529>, [imad.antypas@mail.ru](mailto:imad.antypas@mail.ru)

**Дьяченко Алексей Геннадьевич**, доцент кафедры основ конструирования машин, ФГБОУ ВО «Донской государственный технический университет» (344000, Россия, г. Ростов-на-Дону, пл. Гагарина, д. 1), кандидат технических наук, ResearcherID: O-4796-2018, ORCID: <https://orcid.org/0000-0001-9934-4193>, [dyachenko\\_aleshka@bk.ru](mailto:dyachenko_aleshka@bk.ru)

*Заявленный вклад соавторов:*

Г. Харманда – научное руководство, постановка задачи, определение методологии исследования, критический анализ и доработка решения, компьютерная реализация решения задачи; И. Р. Антибас – анализ теоретических и практических материалов по теме исследования; А. Г. Дьяченко – анализ научных источников по теме исследования, критический анализ и доработка текста.

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